

# Towards a Clean and Sustainable Distributed Energy: The Potential of Integrated PEMFC-CHP

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# Abstract

The use of fossil fuels within the current infrastructure for domestic energy supply is one of the main causes of anthropogenic emissions. The mitigation options to meet the ambitious carbon reduction targets set by the UK government are discussed in this paper, including the use of carbon capture and storage technology, clean renewable energy integration and a proposed system of integrated fuel cell combined heat and power (FC-CHP) technology. Analysis shows that the use of carbon capture and storage (CCS) technology within the current infrastructure can abate half the electricity associated  $CO_2$  emissions; however, this comes at a high cost penalty. The emissions associated with domestic heat cannot be prevented without changes in the energy infrastructure. Hydrogen powered fuel cells can provide clean energy at a range of scales and high efficiencies, especially when employed with a CHP system. However, production of  $CO_2$  free hydrogen is essential for fuel cell technology to contribute substantially to a low carbon economy globally. In this work three methods were investigated for small scale distributed hydrogen production, namely steam methane reforming, water electrolysis and cold plasma jet. The criteria used for comparisons include the associated  $CO_2$  emissions and the cost of energy production. Cold plasma jet decomposition of methane shows a high potential when combined with integrated FC-CHP technology for economically viable and  $CO_2$  free generation of energy, especially in comparison to water electrolysis. Including the value of the solid carbon product makes the plasma system most attractive economically.

Keywords: Clean energy, Hydrogen generation, Cold plasma jet

## 1. Introduction

## 1.1. The hydrogen fuel cell future

The global challenges in energy of growing oil scarcity, security of supply and environmental degradation are well documented, with the drive to develop a cleaner and more sustainable energy infrastructure [1-3] 'The built environment needs to develop more sustainable, less energy-intensive systems......The UK government has identified the house building industry as a key sector in delivering carbon reduction' [4]. Domestic energy consumption for space and water heating, cooking, lighting and appliances is approximately 30 % of total energy use in the UK and contributes 26 % of total UK carbon dioxide emissions, with

average household emissions of 78 kg CO<sub>2</sub>/m<sup>2</sup>/yr. Within a typical UK household, 58 % of the energy is used for space heating, 24 % for hot water and 19 % for cooking, lighting and appliance use [4]. Hydrogen has long been recognised as a key alternative fuel to replace carbon based fossil fuels [5] in conjunction with fuel cell technology [1]. Hydrogen powered fuel cells can provide energy to the transportation sector as well as electricity to a wide range of products, from small portable items such as mobile phones and laptops, to domestic and industrial energy applications [5]. The advantages of hydrogen powered fuel cells include: (i) High efficiency - fuel cells convert fuel to electricity at more than twice the efficiency of internal combustion engines [6], and if heat generated by a fuel cell is utilized in CHP systems, 85% efficiency can be achieved [2]; (ii) Zero emissions - hydrogen fuel cells emit only water and have no pollutant emissions [2]; (iii) Comfort - fuel cells are silent, vibration-free and require very little or no maintenance [6]; (iv) Providing energy at all

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scales - from micro power sources to multi-MW plants [6]. In 2003, the European Commission [5] stated that hydrogen and fuel cells are firmly established as strategic technologies that can meet the following objectives: (i) Maintaining economic prosperity and quality of life, and (ii) Achieving a sustainable energy system that meets the conflicting demands of increased energy supply and security, whilst maintaining costcompetitiveness, reducing climate change, and improving air quality. In 2003 the EC also announced a European hydrogen vision stating that by 2050 a hydrogen orientated economy would be globally implemented [5]. The use of fuel cells could well be more acceptable to residential markets for on-site domestic heat and electricity production, than engine-based technologies involving moving parts, noise and vibration [7]. The use of fuel cells can also reduce environmental emissions: carbon dioxide by 49 %, nitrogen oxide by 91%, carbon monoxide by 68 % and volatile compounds by 93 % as compared with traditional combustion technologies [8]. Fuel cells applied to distributed energy systems have the highest efficiencies (40 - 85%) when compared to conventional means such as the reciprocating diesel engine (35 %), turbine generator (29 - 42 %), photovoltaic (6 - 19 %) and wind turbine (25 %) [9].

### 1.2. The PEMFC-CHP system

The main advantages of Proton Exchange Membrane Fuel cells (PEMFCs) include their reliability and robustness [10]. PEMFCs are 'currently the ones with the most advanced technological development and some cogenerative units are already commercialized' [11]. In its industry review of 2011, Fuel Cell Today wrote that 'in terms of commercial success, the leader by far in terms of units shipments is the PEMFC' contributing 97.03 % of shipments and 73.8 % of MW supplied when compared to other fuel cell types in 2010 [12].

According to Brown et al. [7] Japan will be the first country to make a significant entry into the market for fuel cells for domestic applications. The Japan Gas Association plans to market a high efficiency PEMFC residential cogeneration system with hot water storage tank equipped with back-up burner, a battery for electrical storage and self-diagnostic system; numerous companies are developing residential PEMFC systems [see 8]. To date, more than 13, 307 CHP systems based on PEMFCs and polymer electrolyte fuel cells have been installed in general homes in Japan [13]. In 2006, Aki et al. [14] proposed the implementation of the regional hydrogen energy interchange network (RHEIN) for residential consumption of hydrogen, electricity and heat, with the aim of reducing the cost of installation by sharing of the fuel cells and related equipment between the households. As a follow up, a 2 year demonstration project has been carried out in Osaka City in 2007 - 2009 to evaluate PEM-CHP RHEIN for residential homes [13]. Two cases were examined, namely 6 apartment homes supplied with 3 PEM-CHP units and 4 detached houses supplied with 2 PEM-CHP units; where electricity and water was shared between the homes at the ratio of 1 unit per 2 households. The system consisted of a SMR fuel processor with pressure swing adsorption for purification of hydrogen and PEM fuel cell at maximum supply of 700 W, operated in a grid dependent mode at peak demand. The study has shown that PEM-CHP systems are technologically viable, without any faults or problems experienced during the experimental period. However, problems occurred with high heat loss due to extended hot water sharing pipes. Also, fuel processors showed slow response to the load, were less efficient at partial load and required one hour or more preheating for the catalyst; this

problem was partially overcome by introducing hydrogen storage tanks. Overall, the project has demonstrated a reduction in primary energy consumption and  $CO_2$  emissions by 6 % and 11 %, respectively [13]. In a separate study, Lin et al. [15] also concluded that PEM fuel cell CHP systems are technologically and economically feasible at the current stage, and that additional equipment needed for heat recovery does not contribute much to the overall system financial investment, i.e. does not increase the price significantly.

Compared to other fuel cell types, namely the Solid Oxide Fuel Cell (which can operate on natural gas directly, see [16]), PEMFCs are more demanding since they operate at low temperatures and hence require the feed to be in the form of hydrogen. The presence of CO and CO<sub>2</sub> can have very negative effects on PEM fuel cells; hydrogen dilution with CO<sub>2</sub> can cause a decrease in PEM electrical efficiency by 5 to 10 % [17]. Small scale stationary hydrogen generation is of high importance for the advancement of the already most commercialized domestic PEMFC-CHP systems, when compared to other fuel cell types. At present hydrogen is produced almost exclusively through steam methane reforming (SMR), generating a significant amount of atmospheric CO<sub>2</sub> emissions [18]. Atilla [17] used the Aspen-HYSYS 3.2 process simulation programme to evaluate methane reformers for residential fuel cell PEMFC-CHP systems. The fuel reformers studied were the autothermal reformer, the steam reformer and a partial oxidation reactor. Steam methane reforming was shown to be the most efficient out of the above for the fuel processors and the overall system efficiency. Hence, for hydrogen powered fuel cells to contribute substantially to a low global carbon economy, generation of environmentally friendly hydrogen is necessary. Mitigating options include the use of Carbon Capture and Storage technology and clean renewable technologies to reduce electricity associated emissions, as well as alternative hydrogen generation method, namely pyrolysis.

#### 1.3. Carbon Capture and Storage (CCS)

CCS technology is endorsed by the Intergovernmental Panel on Climate Change and the UK government as a key mitigation option for reducing the emissions from stationary sources such as fossil fuel power stations [19]. CCS includes carbon capture, transportation and storage. Carbon capture involves CO<sub>2</sub> capture at the point of generation, the most common methods being by absorption, adsorption, separation by membranes and cryogenic separation. The captured gas mixture is compressed to a supercritical fluid to be transported by pipeline or ship for storage. Storage options include biological storage, ocean storage and mineralization. The main cost is CO<sub>2</sub> capture ranging from 24 - 52 euro/tonne (equivalent to £ 19 - 43 at the exchange rate of  $\notin$  1 = £ 0.8287). Transportation effects can vary depending on pipeline dimensions, CO<sub>2</sub> pressure and landscape characteristics, costing from 1 - 6 euro/tonne  $(\pounds 0.8287 - 5.0)$  per 100 km pipeline [20]. Different methods of CCS are being addressed, research focusing on economic feasibility and storage safety issues. However, technologies under development focus on large scale CO2 sources such as power stations. Small scale CCS applications have not yet been shown to be viable, major problems occurring in the transport and storage of CO<sub>2</sub> [21]. The UK Department of Energy and Climate Change has recognised that reducing the costs and risks associated with CCS are some of the key challenges for CCS deployment in the UK, even for large scale applications [22]. Reduction of CCS costs mainly lies with the capture technology (60 - 80%) of the total cost) [20]. With regards to CO<sub>2</sub> transport, the UK CCS Roadmap specifies that new pipelines will have to be built, necessitating a whole transport infrastructure. The main challenges lie within storage, including the design, quality of baseline, leakage, monitoring and liability [19], with safety and potential damage to the environment at the top of the list [23].

CCS has not yet been fully demonstrated on a commercial scale, the cost performances reported being based on feasibility studies and pilot projections, which still bear some uncertainty [24]. It is difficult to predict the cost of CCS as it includes the transport and storage of carbon, of which transport is the major variant depending as it does on the siting of the sinks. Studies show that the cost of electricity generation with CCS post 2020 would increase by an average of 45 % [25]. CCS viability for applications in UK electricity generating industries was performed by Element Energy for the Committee on Climate Change [26]. The analysis shows that CCS has the potential to address up to 38 Mt of CO2 emissions per annum in 2030 (decreasing to 37 Mt by 2050) for a cost range of £30 to £150 per tonne of CO<sub>2</sub> abated. The findings also reveal that the capital cost of the addition of post-combustion capture equipment to gas powered stations almost doubles the total capital cost of the plant; additional complications include gaining permission for a CO<sub>2</sub> pipeline route which, combined with other factors is likely to lengthen the overall build time, if not the shut-down period for the power station [26].

#### **1.4.** CO<sub>2</sub> free generation of hydrogen

Hydrocarbon pyrolysis is one alternative method of hydrogen generation, involving a direct decomposition of gaseous hydrocarbons into hydrogen and carbon black [27]. The most promising hydrocarbon is methane [2]. Pyrolysis is optimally environmentally friendly as it does not produce any CO<sub>x</sub> [28,29] and is more economical than SMR with carbon capture [30]. The current decomposition methodology employing catalysts is challenging due to catalyst stability considerations [31]. However, problems associated with catalyst sensitivity and deterioration, can be eliminated or diminished by careful application of plasma technology, thereby achieving higher conversion efficiencies and increased specific productivity [27]. Non-thermal plasmas are especially considered to be very promising for organic synthesis applications; however, the present understanding of plasma chemistry is limited and most of the achievements to date have been based on experimental data [32]. They have been successfully applied to hydrogen production from a variety of feedstock: methane, liquid hydrocarbons and biomass. Non-thermal plasma generation methods, including microwave [33], corona discharge [34] and gliding arc [35] have achieved partial oxidation of methane to generate syngas (carbon monoxide and hydrogen). Similarly, atmospheric pressure microwave discharge [36] and pulsed plasma discharges [37-41] have been successfully applied to direct methane decomposition to hydrogen and carbon. Investigations using plasma assisted steam reforming (methane oxidation by water vapour) have been made with such discharge methods as microwave [42] and pulsed corona [27].

Based on the above rationale, our case studies in this work have focused on comparing *a Cold Plasma Jet* with *SMR* (the most competitive fuel processor) and *Water Electrolysis* (another technology at an R&D stage). The cases are:

- (i) The current stage of hydrogen generation with the carbon charge;
- (ii) Hydrogen generation post 2020 with the integration of CCS;

- (iii) Hydrogen generation post 2035 with the integration of clean renewable energy, &
- (iv) PEMFC-CHP integration for direct electricity and heat generation. The UK National Grid energy supply for 2010 is also presented, showing the issues arising.

The aim of this work is to identify the most economical path to eliminate or reduce  $CO_2$  emissions for hydrogen production applied to a domestic CHP supply chain.

### 2. Methodology

In order to carry out the above case studies certain data inputs and preliminary calculations are necessary. These are presented here.

# 2.1. Data input for national energy supply, emissions and costing calculations

Firstly, energy supply and emissions data for the UK national grid for 2010 [43] are used as given in Table 1.

Table 1: National	grid energy	supply and	$CO_2$	emissions	for	2010
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National Grid (2010)	Elect	Heat		
Primary fuel used	NG	Coal	NG	
Total fuel consumed (GWh)	371,736 <sup>1</sup>	297,301 <sup>1</sup>		
Supplied (gross) (GWh)	171,822 <sup>1</sup>	102,266 <sup>1</sup>		
Transmission and distribution loss (%)	7.	$5^2$		
Efficiency (%)	42.5	34		
Average efficiency (%)	39		90	
Total Domestic supply (GWh)	118 681 <sup>3</sup>		350,635 <sup>4</sup>	
Total domestic supply efficiency (%)	67.6			
Average CO <sub>2</sub> emissions (tonne/GWh)	) 587 <sup>5</sup>		1855	
Domestic CO <sub>2</sub> emissions 2010 (Mt)	69	64.87		
Domestic CO <sub>2</sub> emissions 2010 (wit)	134.53			

All data taken from [61]: <sup>1</sup>p. 143, table 5.6; <sup>2</sup>p. 167, table 6H; <sup>3</sup>p138, table 5.2; <sup>4</sup>p. 112, table 4.2; <sup>5</sup>p. 126, table 5.A.

The primary fuel consumed in the form of natural gas (NG) and/or coal for domestic electricity and heat supplied is calculated using the efficiency factors of 0.39 and 0.9 respectively (energy supplied/efficiency factor), shown in Table 1 as an average efficiency. The total efficiency of energy supply (output energy/total primary input energy) taking into account the transmission and distribution losses is 67.6 %.

The second set of general data inputs are for the carbon, CCS and renewable energy integration cost calculations. These are given in Table 2.

Table 2: Data input for cost calculations (relevant references in text below).

		Cost reported	Cost calculated (£)
Natural gas		€ 0.0465/kWh	0.0385 /kWh
		€ 0.1676/kWh	0.1389 /kWh
Electricites	With TC		0.1465 /kWh
Electricity	With CCS		0.2014 /kWh
	Renewables		0.190 /kWh
Me	ethane		0.0480 /kWh
Traded c	arbon value	£13 ton/CO <sub>2</sub>	0.0130 kg/CO2
Non-tradeo	l carbon value	£55 ton/CO <sub>2</sub>	0.0550 kg/CO <sub>2</sub>
Solid carbon	Low Quality	$\pounds$ 200 ton/C <sub>s</sub>	£ 0.2 kg/Cs
Value	High Quality	£ 1000 ton/Cs	£ 1 kg/Cs

The cost of natural gas and electricity are for household ('enduser') energy prices for November 2011 [44]. Consequent hydrogen production calculations assume that the methane feedstock is via natural gas supply from the grid. The constitution of natural gas is 70-90 %; taking the average 80 %, the price of methane is £ 0.048 per kWh. The Traded Carbon (TC) value is taken for 2010, and under the European Union Emissions Trading Scheme is £13 tonne/CO<sub>2</sub> (£ 0.013 kg/CO<sub>2</sub>) [45]. Power station generated electricity in this scenario is part of the traded scheme, and its cost including the TC charge is £0.1465. The corresponding Non-Traded Carbon (NTC) charge for 2010 under the European Union Emissions Trading Scheme is £55 tonne/CO<sub>2</sub> (£ 0.055 kg/CO<sub>2</sub>). Household emissions from heating and small scale SMR both fall under this scheme [45]. The cost of CO<sub>2</sub> for each system described is equal to the amount of  $CO_2$  released (tonne $CO_2$ ) times the corresponding carbon charge as above (£/tonneCO<sub>2</sub>).

The reduction in efficiency for coal and gas power plants with CCS is approximately 8 %, [24]; hence the net average efficiency for UK grid electricity supply with CCS in 2010 is 31 % (average efficiency of 39 % in Table 1 minus the 8 % reduction). For post 2020 conditions it has been estimated [25] that the cost of electricity generation with CCS will have increased by 45 %. Therefore, it can be reasonably assumed that retail electricity will increase by the same rate to  $\pounds$  0.2014 per kWh, as in Table 2. Again it has been estimated that CCS will be able to process up to 38 Mt of CO<sub>2</sub> emissions per annum by 2030 [26], which is equivalent to 55 % of total electricity related CO<sub>2</sub> emissions for 2010. A US Department of Energy analysis predicts that electricity related CO2 emissions can be reduced by 60 % by 2035 under the Clean Energy Standard. This involves the integration of clean energy: nuclear, hydro, geothermal, municipal waste, solar, wind and biomass [46]. However, this integration will result in a 27 % increase in the electricity price to £ 0.190 per kWh.

The CO<sub>2</sub> emissions released for domestic electricity and heat supplied amount to energy supplied (GWh) times the average CO<sub>2</sub> emissions (tonne/GWh), data given in Table 1. Hence, the total CO<sub>2</sub> released in UK for the whole year in 2010 by a) domestic electricity consumption is 69.66 Million tonnes (Mt); these are accounted as TC emissions with a total carbon cost of £905.58 Millions. The corresponding CO<sub>2</sub> emissions from b) domestic heat consumption are 64.87 Mt; these are accounted as NTC emissions, the carbon cost being £ 3,568 Millions. The retail costs of electricity and natural gas are given in Table 2 as £0.1389 and £0.0385 per kWh respectively. The total annual cost is based on the retail cost of the energy supplied, excluding the carbon cost.

Finally, the Cold Plasma Jet has the potential to generate not only hydrogen, but solid carbon as well. This can be harvested and used in a variety of industrial processes; it has a commercial value of  $\pounds$  200 to  $\pounds$  1000 /tonne depending on the quality [47]. Crystalline carbon structures such as nanotubes are referred to as High Quality Solid Carbon (HQSC), where Low Quality Solid Carbon (LQSC) is the amorphous carbon (e.g. carbon black).

#### 2.2. Hydrogen generation cost

The alternative methods of reforming methane or natural gas will require different forms and quantities of energy and will generate different amounts of hydrogen. The cost of generation of hydrogen is the sum of the price of the input fuels, in the form of electricity and or methane/natural gas. For an SMR unit the Non-Traded Carbon Charge (NTCC) is also added. The cost is calculated as follows:

$$CkgH_2 = F_i \times C_i + F_{elec} \times C_{elec} + X_{CO_2} \times NTCC$$
(1)

The consumption of fuel, whether methane or natural gas, to generate 1 kg of hydrogen is calculated by dividing the fuel consumption rate (kg/s) by the hydrogen production rate (kg/s); the obtained value (kg) is then multiplied by the HHV of the fuel (kJ/kg) and divided by the factor of 3600 to acquire  $F_i$  (kWh). The consumption of electric energy  $F_{elec}$  is calculated by dividing the power rating of the reformer (kWh) by the hydrogen production rate (kg/s). The amount of CO<sub>2</sub> generated by the SMR unit (kg) is calculated by dividing the CO<sub>2</sub> production rate (kg/s) by the hydrogen generation rate (kg/s). The cost of electricity  $C_{elec}$  is reported in Table 2 for all case studies, i.e. with TC, with CCS and integrated renewables.

### 2.3. Reformer input data

The commercial SMR unit (Helbio APS 1000) generates 2.97 x  $10^{-4}$  kg/s hydrogen (1.2 m<sup>3</sup>/h reported) at a natural gas consumption rate of 1.02 X 10 <sup>-4</sup> kg/s (0.43 Nm<sup>3</sup>NG/Nm<sup>3</sup>H<sub>2</sub> reported) and power rating of 0.096 kW. Reformate stream constituents by volume are 74 % H<sub>2</sub> 24 % CO<sub>2</sub> and 2 % CH<sub>4</sub> with equivalent CO<sub>2</sub> production rate of 7.14 kg per kg H<sub>2</sub> [48].

The domestic electrolyser technology is at the 'R&D' stage. The data used for this work was reported for the DOE by EPRI funded research [49] at 6.3 kW power rating for hydrogen production rate of 3.47 x  $10^{-5}$  kg/s (specified as 1 kg/day at 8h/day operation).

Cold Plasma conversion of methane to hydrogen is also at the R&D stage. The data used for this work are from the non-thermal plasma jet experiments reported by Li et al. [38]. The methane consumption rate is calculated using the reported mass flow rate given of 880 ml/min and methane conversion rate of 60.97 % [38]:

$$c_{CH_4} = n_{CH_4} \times Conv_{CH_4}$$
(2)

The hydrogen generation rate is calculated from the reported hydrogen selectivity of 89.3 % [38] and the methane conversion rate:

$$\mathbf{p}_{\mathrm{H}_{2}} = \mathbf{c}_{\mathrm{CH}_{4}} \times 2 \times \mathbf{S}_{\mathrm{H}_{2}} \tag{3}$$

The summary of the important parameters for SMR, water electrolysis and cold plasma jet specifications is given in Table 3, where the fuel conversion efficiency for the system is calculated as follows:

$$E = \frac{p_{H_2} \times HHV_{H_2}}{c_i \times HHV_i + W} \times 100$$
(4)

Table 3: Data inputs for SMR, WE and CPJ reformers

	SMR	WE	СРЈ
Power rating (kW)	0.096	6.3	0.07
Fuel consumption (kg/s)	1.02 X 10 <sup>-4</sup>		6.4 X 10 <sup>-6</sup>
H <sub>2</sub> generation (kg/s)	2.97 X 10 <sup>-4</sup>	3.47 X 10 <sup>-5</sup>	1.43 X 10 <sup>-6</sup>
CO <sub>2</sub> (kg CO <sub>2</sub> /kg H <sub>2</sub> )	7.14		
Conversion efficiency (%)	77.1	78.1	47.7

## 2.4. FC-CHP system specifications

The final comparison study involving an integrated Fuel Cell/CHP system (FC-CHP), uses as input data the specifications for the commercial PEMFC CHP system developed by Ballard MK5-E PEMFC stack [50]. These, together with other (calculated) data are given in Table 4.

## Table 4: Fuel Cell CHP system

Fuel Cell Specifications (Ballard MK5-E PEMFC stack)					
Temperature	70 °C				
Max output electric	4 kW				
Max thermal recovered	3 kW				
Power to heat ratio	1.33				
Electrical efficiency	45 %				
Thermal efficiency	35 %				
CHP efficiency	80 %				

Electricity generation from 1 kg hydrogen input using the data from Table 4 is calculated as follows:

$$W = E \times HHV_{H_2} \times p_{H_2}$$
(5)

and is equal to 17.735 kWh. The power to heat ratio is 1.33 hence, the heat generated is 13.301 kWh.

## 3. Results and Discussion

## 3.1. UK National grid 2010 conditions

Figure 1 summarises diagrammatically the UK energy supply from the national grid in 2010 together with the costing and the associated  $CO_2$  emissions calculated based on the discussion and information in section 2.1.



# Total $CO_2$ emissions: 134.53 Mt $CO_2$ Total carbon cost: £ 4, 474 Millions

Figure 1: Domestic energy supply from the National Grid in 2010 and associated carbon dioxide emissions. Notes: (i) the costing is for the retail price for total energy consumed; (ii) the heat and electricity cost does not include the stated carbon charge

Using the same 2010 data, but incorporating CCS into the system, leads to Figure 2. If CCS becomes commercially viable as planned post 2020, over half of the emissions from the UK electricity supply sector can be eliminated. However, this brings a financial penalty to the power station and the consumer. The overall process efficiency is decreased and the

retail cost of electricity increases steeply. As discussed in the introduction, since CCS is not viable at small scales in the foreseeable future, the emissions from domestic heat generation cannot be reduced by CCS. The integration of clean energy can reduce the emissions by 60 % at the penalty of a 27 % increase in the price of electricity to £0.190 per kWh.



Figure 2: Domestic energy supply from the National Grid using 2010 data with future anticipated CCS. Notes: (i) the costing is for the retail price for total energy consumed; (ii) the heat and electricity cost does not include the stated carbon charge

# **3.2.** Comparison of current hydrogen generation systems: effect of solid carbon credit

The rationale of this study is to compare the three hydrogen generation alternatives of Steam Methane Reforming (SMR), Water Electrolysis (WE) and Cold Plasma Jet (CPJ). Calculations for current conditions (data for 2010) *and taking hydrogen as the end product*, leads to the results shown in Figure 3 and Table 5. CPJ is competitive with SMR in terms of  $CO_2$  emissions. The overall hydrogen cost is lowest using SMR, with CPJ coming second.

According to Bartels et al. [51] the approximate cost of large scale hydrogen production using SMR was 2.48 - 3.17 US \$/kg of hydrogen in 2007 (equivalent to £1.6 - 2.05 at exchange rate of \$1 = £0.6464). For commercial large scale WE the cost was estimated to be in excess of 8 US \$/kg [52] (equivalent to £5.17). As expected, small scale hydrogen generation using both SMR and WE is a more costly process than for large scale generation. However, it is also necessary to consider the requisite extra costs involved in implementing a new hydrogen infrastructure for transport, and storage for supplying domestic districts with hydrogen for FC-CHP. Further, the emissions from a large scale SMR plant have been estimated to be 13.7 kg CO<sub>2</sub> per kg of hydrogen [53], while the small scale commercial SMR unit in this study only generates 7.67 kg CO<sub>2</sub> per kg hydrogen in total.

When the value of the solid carbon product of CPJ [47] is taken into account, the effective hydrogen cost reduces from 5.304 (no credit) to 4.704 and 2.304 for LQSC and HQSC respectively. LQSC and HQSC correspond to the respective levels of £0.2 and £1 per kg C<sub>s</sub> of Table 2. The HQSC value makes CPJ directly competitive with SMR. *The striking effect of C<sub>s</sub> credit (especially for HQSC) holds for all following cases of this study.* WE shows substantially lower potential than CPJ in terms of hydrogen generation cost and associated CO<sub>2</sub> emissions.

Table 5	: Hydrogen	generation	under	current	conditions
		<b>0</b> · · · · ·			

	SMR	WE		СРЈ		
	SMR	WE		LQSC	HQSC	
Conversion Efficiency (%)	77.7	78.1	47.7	47.7	47.7	
System Efficiency (%)	75.6	30.45	37.9	37.9	37.9	
Hydrogen cost (£/kg)	2.442	7.388	5.304	4.704	2.304	
CO <sub>2</sub> emissions (kg CO <sub>2</sub> /kg H <sub>2</sub> )	7.67	29.60	7.98	7.98	7.98	

# **3.3.** Comparison of hydrogen generation systems: post-2020 scenario with CCS

For a post-2020 scenario allowing for anticipated CCS, results of the comparative system analysis of the alternatives are shown in Figure 4 and Table 6.



Figure 3: Summary diagrams for system analysis for hydrogen generation under current conditions, carbon charges included



Figure 4: Hydrogen generation post 2020 with CCS.

Table 6: Hydrogen generation post 2020 with CCS

	SMR	WE		СРЈ	СРЈ	
		WE		LQSC	HQSC	
Conversion Efficiency (%)	77.7	78.1	47.7	47.7	47.7	
System Efficiency (%)	74.8	24.2	34.9	34.9	34.9	
Hydrogen cost (£/kg)	2.495	10.320	6.098	5.498	3.098	
CO <sub>2</sub> emissions (kg CO <sub>2</sub> /kg H <sub>2</sub> )	7.38	13.32	3.59	3.59	3.59	

The addition of CCS has a very small impact on SMR as the electricity consumption is very low and the majority of the emissions associated are from the SMR itself. Since the CO<sub>2</sub> emissions for WE and CPJ are only electricity related, in both cases a 55 % decrease is seen. For this scenario, though, the hydrogen generation cost for WE increases drastically by nearly £ 3 per kg H<sub>2</sub> as all of the primary energy for WE comes in the form of electricity. The hydrogen cost using CPJ only increases by £ 0.806 per kg H<sub>2</sub> as CPJ is not primarily electricity dependent, the majority of energy used being in the form of methane. CO<sub>2</sub> emissions for CPJ in this scenario are nearly half those of SMR; for WE the CO<sub>2</sub> emissions are again the highest.

# **3.4.** Comparison hydrogen generation systems: post-2035 scenario with renewable integrated electricity generation

Another important possible scenario is for 2035 when the electricity system is planned to be integrated with renewable sources. Results of the system analysis are shown in Figure 5 and Table 7. With this scenario little effect is seen for the SMR system vis a vis the post-2020 scenario but WE and CPJ both have somewhat improved with lower emissions and cost.

Fable 7: Hydrogen gene	ration post 2035	with clean r	enewable
energy integration			

	SMR	XX/E		СРЈ	
	SMR	WE		LQSC	HQSC
Conversion Efficiency (%)	77.7	78.1	47.7	47.7	47.7
System Efficiency (%)	77.4	60.5	45.6	45.6	45.6
Hydrogen cost (£/kg)	2.485	9.736	5.937	5.337	2.937
CO <sub>2</sub> emissions (kg CO <sub>2</sub> /kg H <sub>2</sub> )	7.35	11.84	3.19	3.19	3.19



Figure 5: Hydrogen generation post 2035 with clean renewable energy integration

# **3.5.** Comparison of hydrogen generation systems: combination of an integrated FC-CHP system

The most important requirements for stand-alone power generation are the independence of the system from the electricity grid and the use of available fuels and infrastructure such as natural gas [48]. Since the electricity consumption for both the SMR and CPJ is lower than that generated by a fuel cell, using a combined PEMFC-CHP system, means that SMR and CPJ can be self sustained and decentralised from the electricity grid. Results of the system analysis are shown in Figure 6 and Table 8. The CPJ system is convincingly the most attractive:  $CO_2$  emissions have been removed completely and energy generation costs for the HQ  $C_s$  case are better than onequarter that for SMR.

In summary CPJ handsomely outperforms the current commercial SMR and is very substantially better than WE. With the production of High Quality carbon, the cost of energy using CPJ is 4 times lower when compared to the SMR system.



Figure 6: Summary of the system analysis with integrated FC-CHP system

	Table 8:	System	analysis	with	integrated	FC-CHP
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	SMR	WE		СРЈ	
		WE		LQSC	HQSC
Conversion Efficiency (%)	77.7	78.1	47.7	47.7	47.7
System Efficiency (%)	60.5	24	25	25	25
Energy Cost (£/kWh)	0.077	0.237	0.190	0.156	0.018
CO <sub>2</sub> emissions (kg CO <sub>2</sub> /kg H <sub>2</sub> )	7.14	29.6	0	0	0

#### 3. Conclusions and future work

While the UK national grid operates at a high overall efficiency of 67 % for supplying domestic electricity and heat, even with the anticipated use of CCS technology, emissions from domestic heat generation cannot be eliminated.

For all scenarios analysed, CPJ is more competitive than WE in hydrogen cost and  $CO_2$  emissions. Indeed, combining CPJ and FC-CHP can eliminate emissions altogether. CPJ also produces potentially considerably valuable solid carbon and means the technology of CPJ closely competes economically with that of commercialised SMR in terms of hydrogen generation costs. *If*  high quality carbon is produced, CPJ integrated with FC-CHP is not only emission free, but substantially out-competes SMR on the cost of energy. This is a most attractive prospect, considering plasma technology is still at the R&D stage.

Overall, it is clear that distributed hydrogen generation could become very competitive, with CPJ having a high potential for economic and clean energy generation. An important final point is this: given that the CPJ system, unlike the SMR and WE systems, is emission-free in terms of the atmosphere, it is not sensitive to future political and technological uncertainties and decision changing in  $CO_2$ -related costing.

Future system analysis work could include a feasibility study for applying the FC-CHP system to meet the daily loads for domestic electricity and heat in the UK as a whole. Experimental work should include developing a non-thermal plasma reactor to reduce electrical power consumption and enhance overall efficiency. Different electrode configurations and designs should be tested to optimise hydrogen production and ensure effective solid carbon removal.

## Nomenclature

Conv	Conversion rate of a compound (%)
С	Cost (£)
c	Consumption rate of fuel (kg/s)
Е	Energy efficiency (%)
F	Fuel (kWh)

- HHV Higher heating value (kJ/kg)
- n Mass flow rate of a compound (kg/s)
- W Electric energy (kJ/s)
- p Production rate of fuel (kg/s)
- S Selectivity (%)
- X Amount of compound to generate 1 kg H<sub>2</sub> (kg)
- Y Amount of fuel to generate 1 kg H<sub>2</sub> (kWh)

### Subscripts

- CH<sub>4</sub> Methane
- CO<sub>2</sub> Carbon dioxide
- elec Electrical (kWh)
- H<sub>2</sub> Hydrogen
- i Fuel: methane or natural gas

### Abbreviations

- CCS Carbon Capture and Storage
- CHP Combined Heat and Power
- CPJ Cold Plasma Jet
- FC Fuel Cell
- HQSC High Quality Solid Carbon
- LQSC Low Quality Solid Carbon
- Mt Million tonnes

- NG Natural Gas
- NTC Non-Traded Carbon
- PEMFC Proton Exchange Membrane Fuel Cell
- R&D Research and Development
- RHEIN Regional Hydrogen Energy Interchange Network
- SMR Steam Methane Reforming
- TC Traded Carbon
- WE Water Electrolysis

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